

*Truss Topology Optimization under Constraints
on Number of Different Design Variables*

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June 11, 2015

constraint on “# of different design variables”

- a new modeling of design constraints
 - optimal standardization / optimal grouping
- a global optimization approach
 - MISOCP (mixed-integer second-order cone programming)

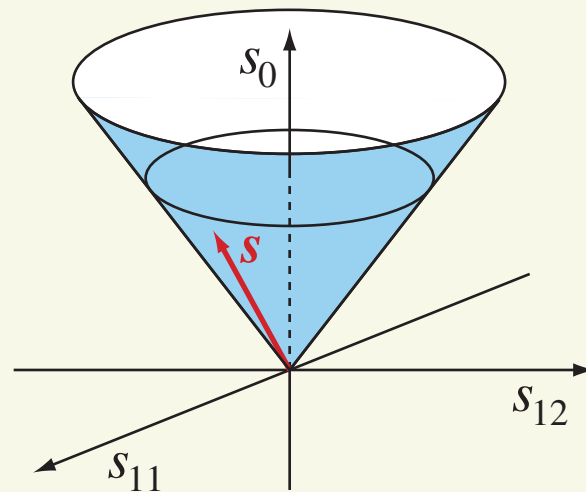
second-order cone programming

- SOCP:

$$\begin{array}{ll} \text{Min.} & \mathbf{c}^\top \mathbf{x} \\ \text{s. t.} & \mathbf{p}_i^\top \mathbf{x} + q_i \geq \|\mathbf{c}_i - A_i \mathbf{x}\| \quad (i = 1, \dots, m) \end{array}$$

- nonlinear convex optimization
- primal-dual interior-point method

- SOC:



MISOCP (= mixed-integer second-order cone programming)

- “integrality” + SOC:

$$\begin{aligned} \text{Min.} \quad & \mathbf{c}^\top \mathbf{x} \\ \text{s. t.} \quad & \mathbf{p}_i^\top \mathbf{x} + q_i \geq \|\mathbf{c}_i - A_i \mathbf{x}\| \quad (i = 1, \dots, m) \\ & x_1, \dots, x_r \in \{0, 1\} \\ & x_{r+1}, \dots, x_n \in \mathbb{R} \end{aligned}$$

- some discrete variables & some continuous variables
- relax $x_j \in \{0, 1\}$ as $0 \leq x_j \leq 1 \rightarrow$ SOCP
 - solvable with, e.g., a branch-and-bound method

MISOCP (= mixed-integer second-order cone programming)

- “integrality” + SOC:

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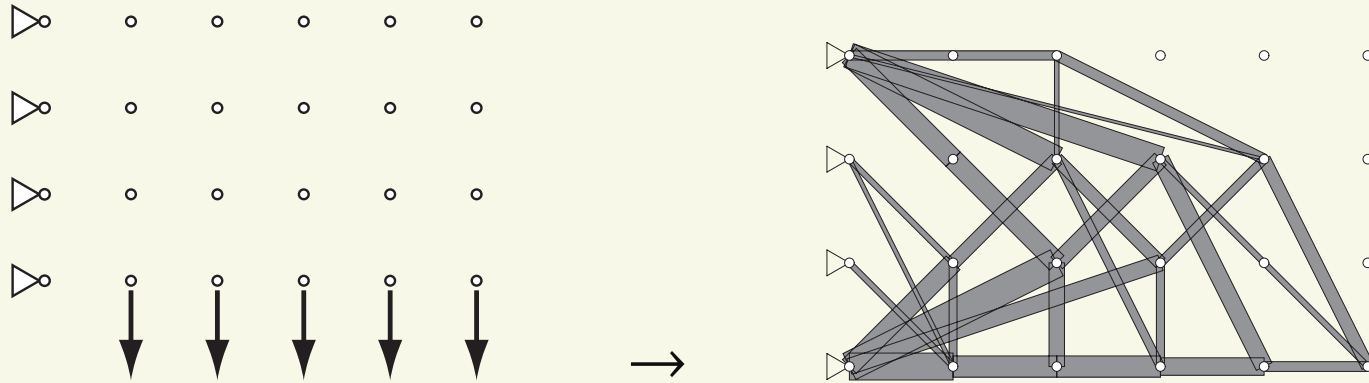
- some discrete variables & some continuous variables
- relax $x_j \in \{0, 1\}$ as $0 \leq x_j \leq 1 \rightarrow$ SOCP
 - solvable with, e.g., a branch-and-bound method
- higher modeling ability than MILP
- well-developed solvers
 - commercial: CPLEX, Gurobi Optimizer, XPRESS
 - non-commercial: SCIP [[Achterberg '09](#)]

m-i prog. in structural optimization

- m-i linear prog.:
 - continuum, absence (0) or presence (1) of elements [Stolpe & Svanberg '03]
 - truss, discrete c.-s. areas [Rasmussen & Stolpe '08] [Mela 14]
 - tensegrity (cable–strut structure) [K. '12, '13]
- m-i nonlinear prog.:
 - truss, discrete c.-s. areas [Achtziger & Stolpe '07] [Cerveira, Agra, Bastos & Gromicho '13] [Stolpe '14]
 - truss, continuous c.-s. areas [Ringertz '86] [Ohsaki & Katoh '05]
 - link mechanism [Stolpe & Kawamoto '05]
- m-i quadratic prog.:
 - truss, discrete c.-s. areas [Achtziger & Stolpe '09]

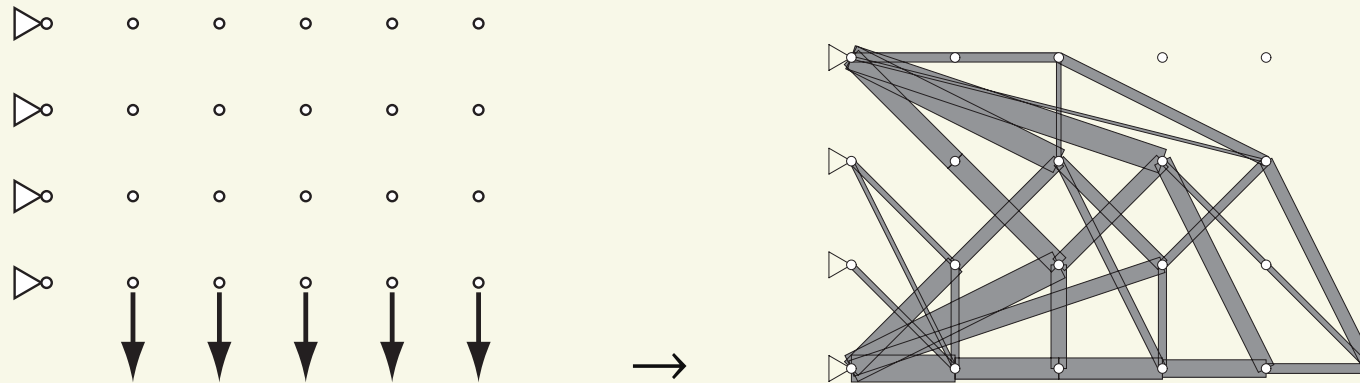
motivation: truss optimization

- conventional compliance optimization:



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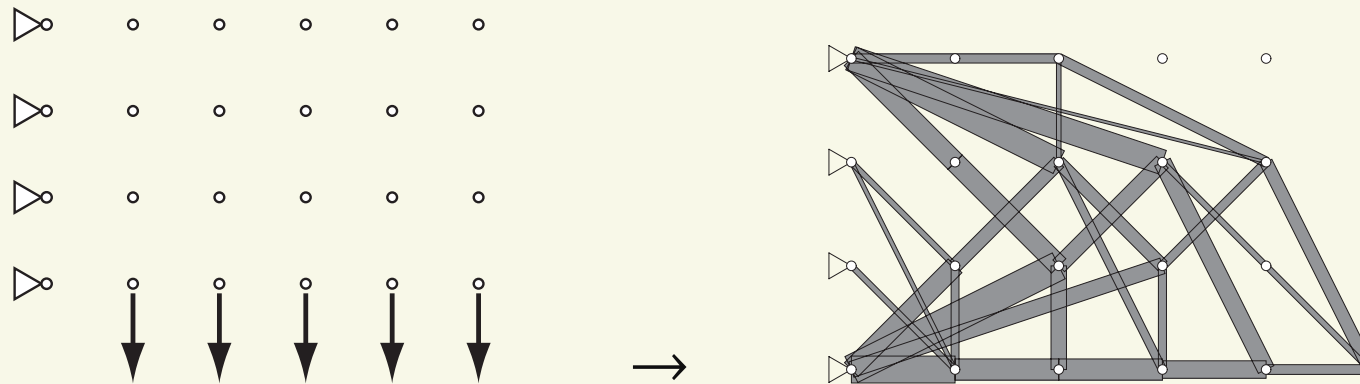
- conventional compliance optimization:



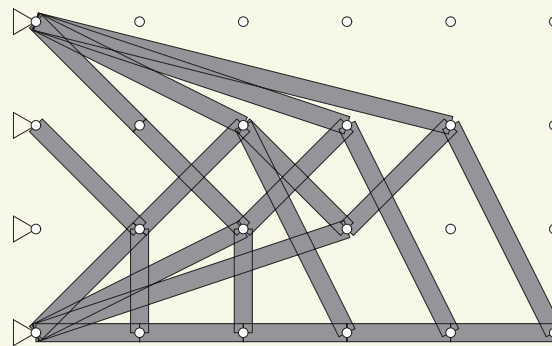
- (almost) all members have **different** cross-sectional areas
 - 29 members have 25 different c-s areas
 - practically unrealistic

motivation: truss optimization

- conventional compliance optimization:



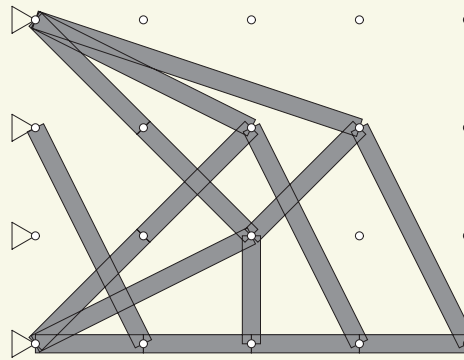
- opt. sol. w/ uniform c-s areas:



- high manufacturability
- → new constraint: “# of different c-s areas” $\leq n$
- uniform $\Leftrightarrow n = 1$

uniformity constraint ($n = 1$)

- two decisions:
 - Determine whether member e exists or vanishes. [combinatorial]
 - Determine the opt. val. for the common c-s area. [continuous]



→ Both are addressed simultaneously.

uniformity constraint ($n = 1$)

- two decisions:
 - Determine whether member e exists or vanishes. [combinatorial]
 - Determine the opt. val. for the common c-s area. [continuous]
- x_1, \dots, x_m : member c-s areas
 - additional variables: $t_1, \dots, t_m \in \{0, 1\}, y \in \mathbb{R}$

uniformity constraint ($n = 1$)

- two decisions:
 - Determine whether member e exists or vanishes. [combinatorial]
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- x_1, \dots, x_m : member c-s areas

- additional variables: $t_1, \dots, t_m \in \{0, 1\}, y \in \mathbb{R}$

$$x_e = \begin{cases} y & \text{if } t_e = 1 & \text{[exists]} \\ 0 & \text{if } t_e = 0 & \text{[vanishes]} \end{cases}$$

- reformulation to linear inequalities:

$$\begin{aligned} 0 &\leq x_e \leq x^{\max} t_e \\ |x_e - y| &\leq x^{\max} (1 - t_e) \end{aligned}$$

- $y \in \mathbb{R}$ is a continuous design variable.
- x^{\max} : a constant (upr. bd. for x_e)

generalization: up to n different values

- two decisions:
 - Determine optimal values for c-s areas, y_1, \dots, y_n .
 - Determine which x_e chooses out of $0, y_1, \dots, y_n$.

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- 0-1 variables

- $s_{e1}, \dots, s_{en} \in \{0, 1\}$: selection among y_1, \dots, y_n

$$x_e = y_j \iff s_{ej} = 1$$

- $t_e \in \{0, 1\}$: existence/absence of member e

$$t_e = s_{e1} + \dots + s_{en}$$

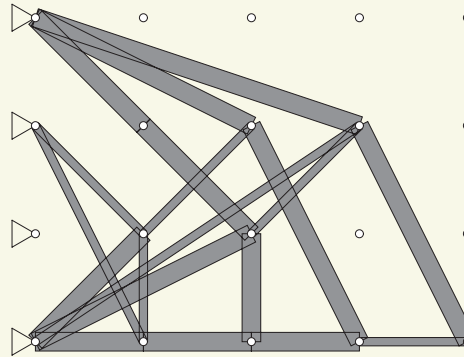
- reformulation to linear inequalities:

$$0 \leq x_e \leq x^{\max} t_e$$
$$|x_e - y_j| \leq x^{\max} (1 - s_{ej})$$

- $y_1, \dots, y_n \in \mathbb{R}$ are continuous design variables

meaning of the constraints

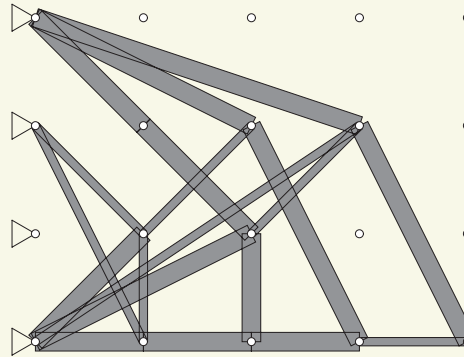
- example: $n = 2$



opt. sol.

meaning of the constraints

- example: $n = 2$



- Members are divided into...
 - set (A): Members whose c-s areas are 0.
 - set (B): Members whose c-s areas are y_1 .
 - set (C): Members whose c-s areas are y_2 .
- two factors:
 - To which set member e belongs?
 - What are the optimal values for y_1 & y_2 ?

[optimal grouping]

[optimal sizing]

for compliance optimization...

- conventional compliance optim.:

Min. (compliance)

s. t. (vol. cstr.), (c-s area ≥ 0)

for compliance optimization...

- conventional compliance optim.:

$$\begin{array}{ll} \text{Min.} & (\text{compliance}) \\ \text{s. t.} & (\text{vol. cstr.}), (\text{c-s area} \geq 0) \end{array}$$

- (compliance) = $2 \times$ (complementary energy)

- cstr.: force-balance eq.

→ SOCP

[Ben-Tal & Nemirovski '01] [Jarre, Kočvara & Zowe '98]

for compliance optimization...

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→ SOCP

[Ben-Tal & Nemirovski '01] [Jarre, Kočvara & Zowe '98]

- compliance optim. w/ cstr. on # of different c-s areas

→ MISOCP (!)

- It can be solved globally.

basis: SOCP for compliance optimization

- SOCP formulation:

$$\begin{aligned} \text{Min.} \quad & 2(w_1 + \cdots + w_m) \\ \text{s. t.} \quad & w_e + x_e \geq \left\| \left[\begin{array}{c} w_e - x_e \\ \sqrt{2l_e/E}q_e \end{array} \right] \right\| \quad (\spadesuit) \\ & \sum_{e=1}^m q_e \mathbf{b}_e = \mathbf{f}, \quad (\text{vol. cstr.}) \end{aligned}$$

[Jarre, Kočvara & Zowe '98] [Ben-Tal & Nemirovski '01]

- variables:

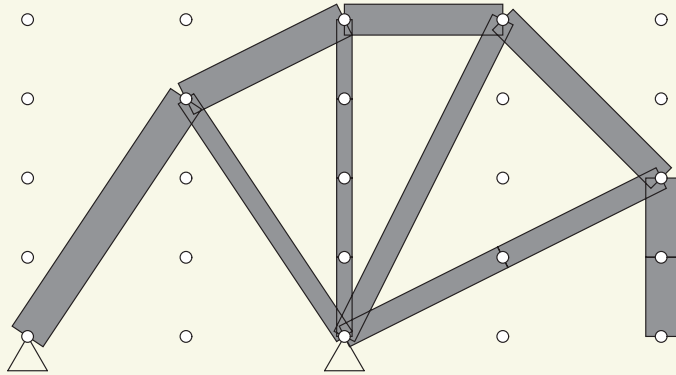
x_e : c-s area, q_e : axial force, w_e : complementary strain energy

- If $x_e > 0$,

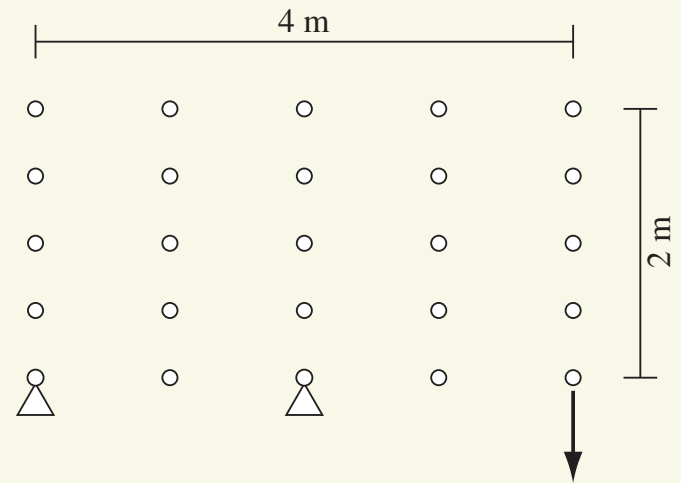
$$(\spadesuit) \Leftrightarrow w_e \geq \frac{1}{2} \frac{l_e}{E x_e} q_e^2$$

i.e., def. of complementary strain energy.

ex.) 200-bar truss

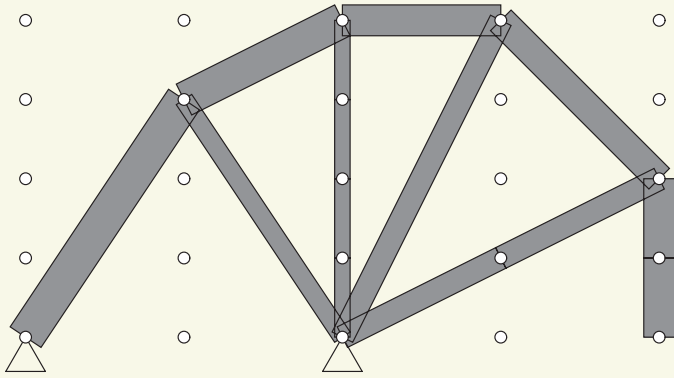


continuous optim.

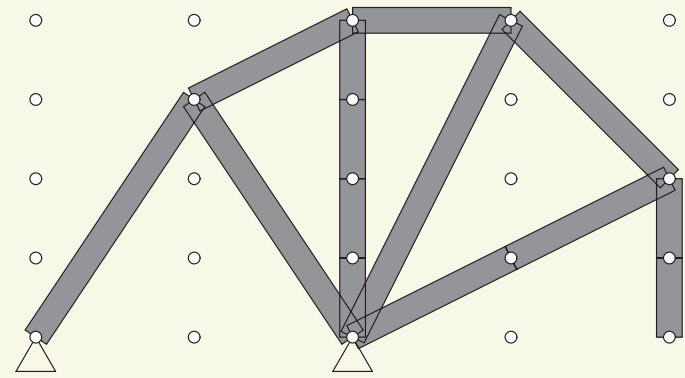


ground structure

ex.) 200-bar truss

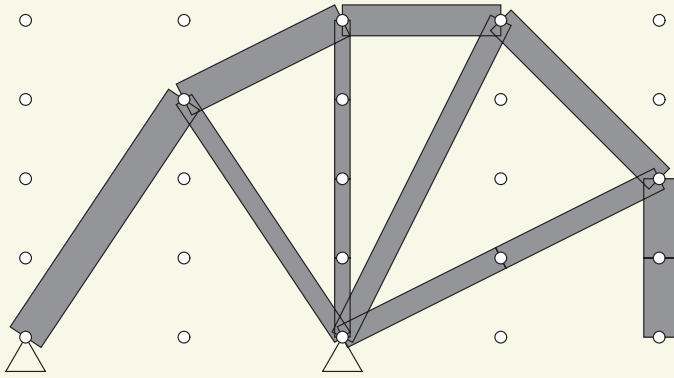


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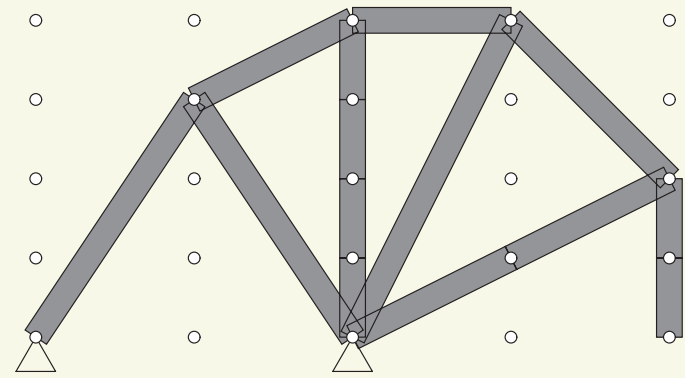


$n = 1$: uniform

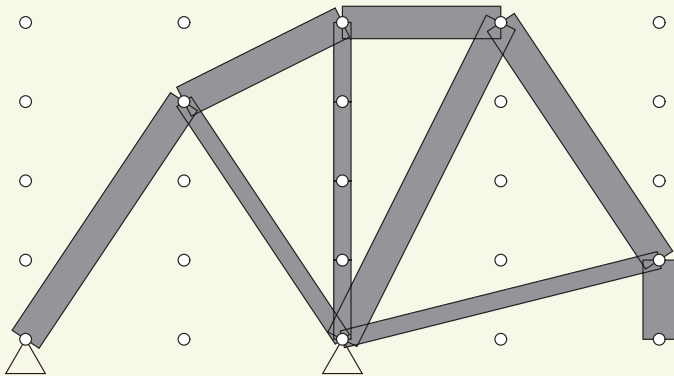
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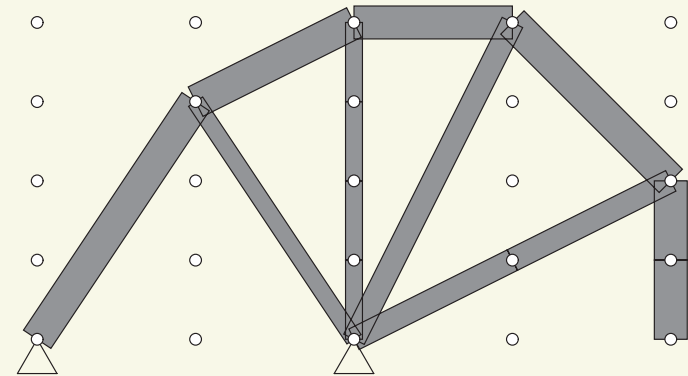
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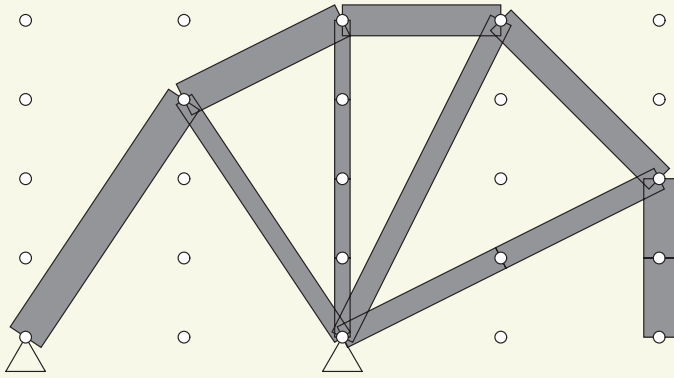


$n = 2$: two groups

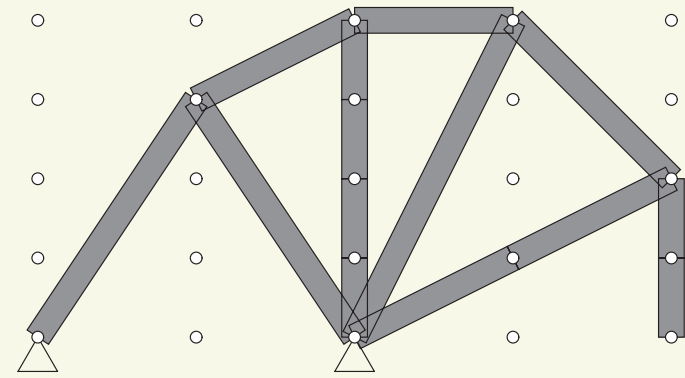


$n = 3$: three groups

ex.) 200-bar truss



continuous optim. 462.59 J

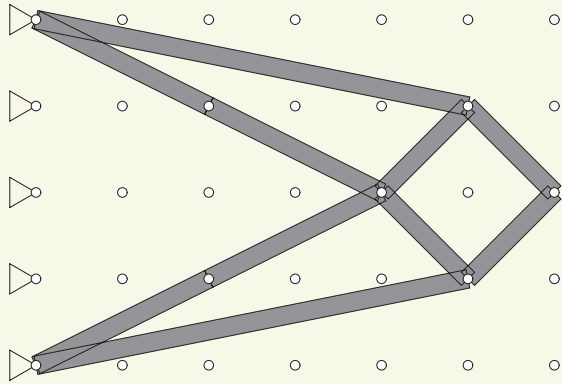


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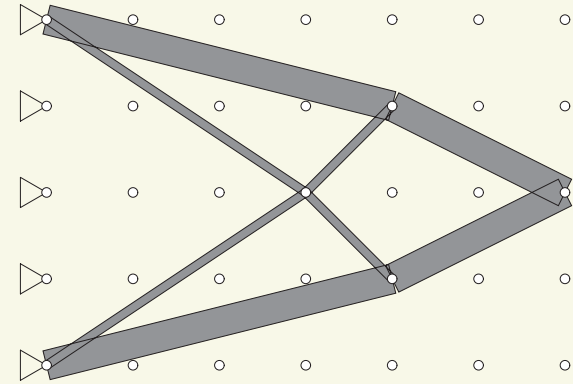
n	Obj. (J)	Areas (mm ²)			Time (s)	# of 0-1 vrbs.
		y_1	y_2	y_3		
1	497.38	1095.15	—	—	13.2	200
2	469.55	1380.90	736.34	—	16.2	400
3	465.63	1403.07	976.98	721.14	33.5	600

- Member standardization is realized with small increase of opt. val.

ex.) cantilever truss



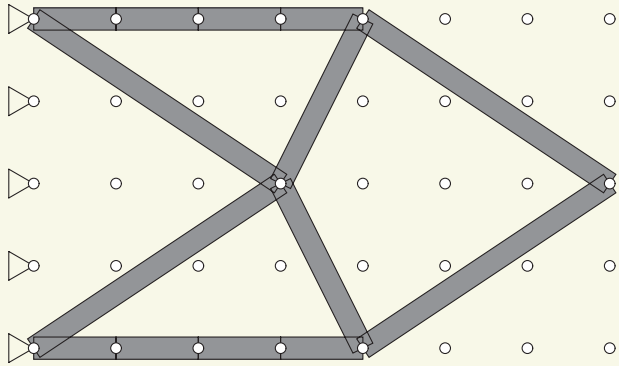
$$(N_X, N_Y) = (6, 4), n = 1$$



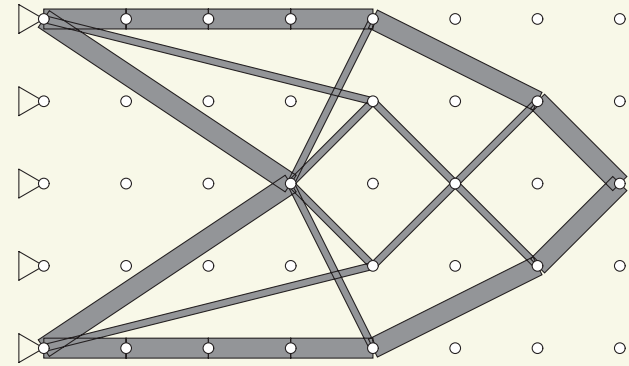
$$(N_X, N_Y) = (6, 4), n = 2$$

(N_X, N_Y)	n	# of membs.	# of 0-1 vrbs.	Time (s)
(6, 4)	1	386	386	202.1
(6, 4)	2	386	772	137.7
(7, 4)	1	503	503	278.2
(7, 4)	2	503	1006	1,015.8
(5, 6)	1	559	559	2,778.5
(6, 6)	1	748	748	24,850.6 (< 7 h)

ex.) cantilever truss



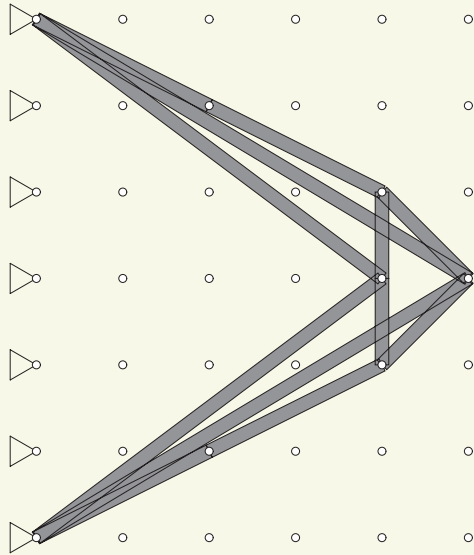
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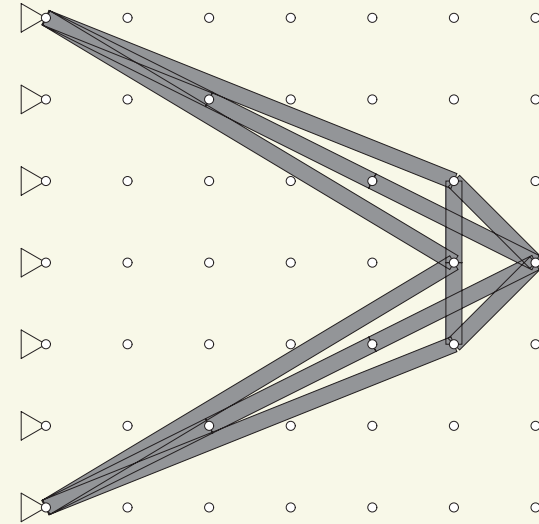
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ex.) cantilever truss



$(N_X, N_Y) = (5, 6), n = 1$



$(N_X, N_Y) = (6, 6), n = 1$

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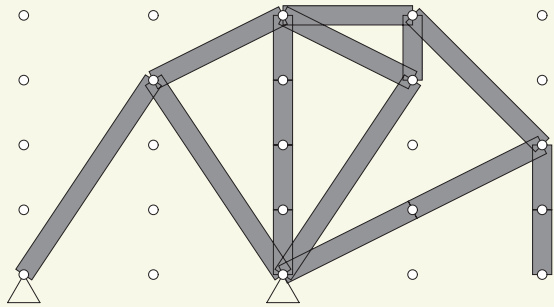
a by-product

- MISOCP is efficient for “discrete truss optimization”,...
 - ...compared with MILP/MIQP.
 - (!) MILP [Rasmussen & Stolpe '08] & MIQP [Achtziger & Stolpe '09] can handle, e.g., stress cstr.

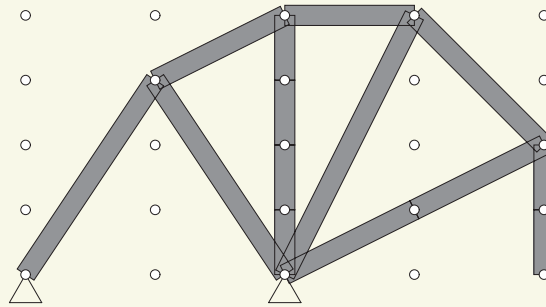
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 - (!) MILP [Rasmussen & Stolpe '08] & MIQP [Achtziger & Stolpe '09] can handle, e.g., stress cstr.
- comparison:
 - Choose c.-s. areas as $x_1, \dots, x_m \in \{0, \bar{\xi}_1, \bar{\xi}_2, \dots, \bar{\xi}_r\}$,
 - w/o cstr. on # of different c-s areas
 - compliance optim.
 - $m = 200, r = 1, 2, 3$:
 - “MISOCP < 20 s” vs. “MILP, MIQP > 24 h”
 - MILP & MIQP use big-M.
 - Relaxation of MISOCP has nonlinear (convex) constraints.

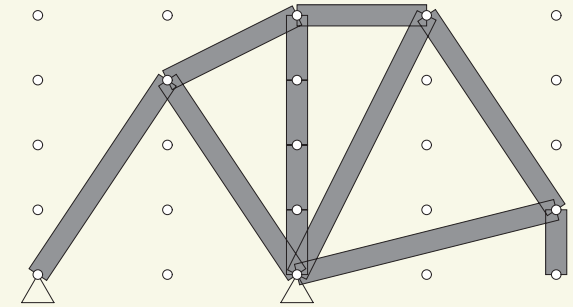
ex.) 200-bar truss: discrete optimization



$$x_e \in \{0, 1000\}$$

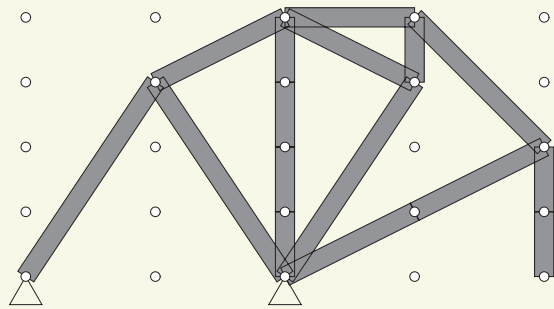


$$x_e \in \{0, 1050\}$$

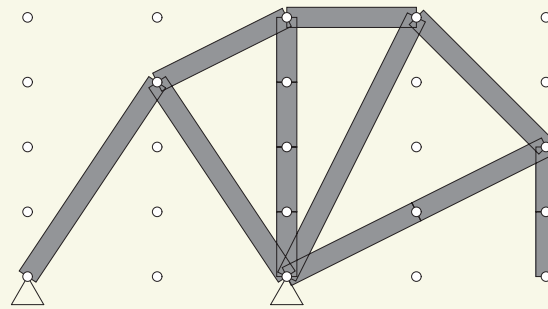


$$x_e \in \{0, 1100\}$$

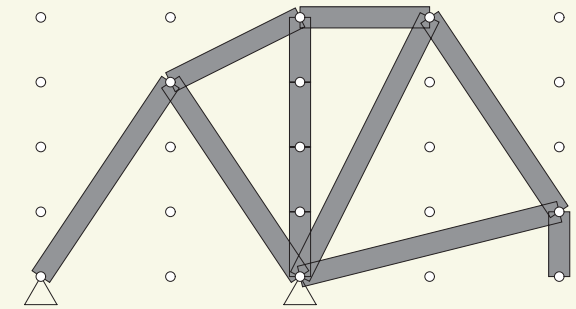
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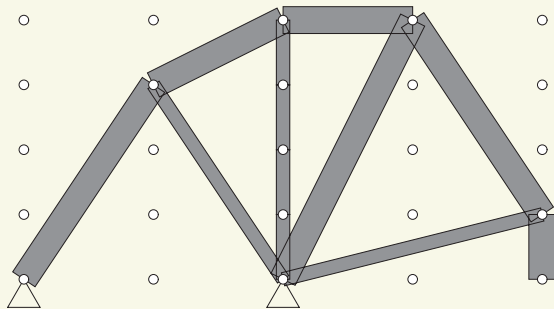
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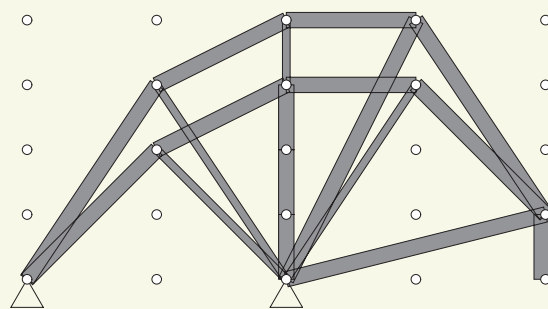
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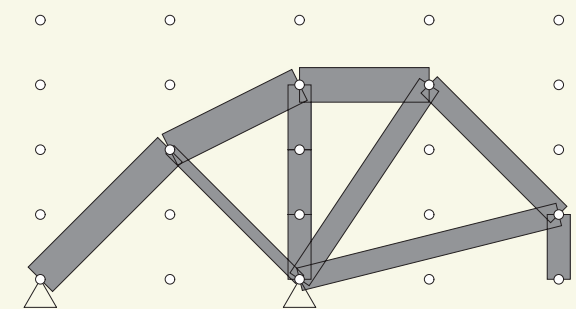
$$x_e \in \{0, 1100\}$$



$$x_e \in \{0, 700, 1400\}$$



$$x_e \in \{0, 600, 1200, 1800\}$$

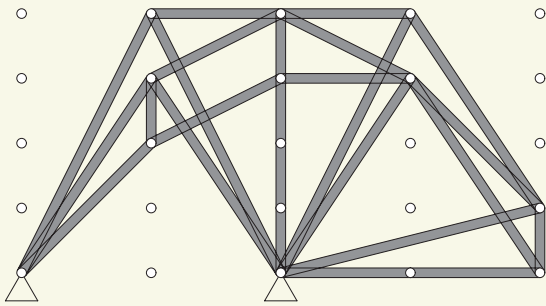


$$x_e \in \{0, 400, 800, 1200\}$$

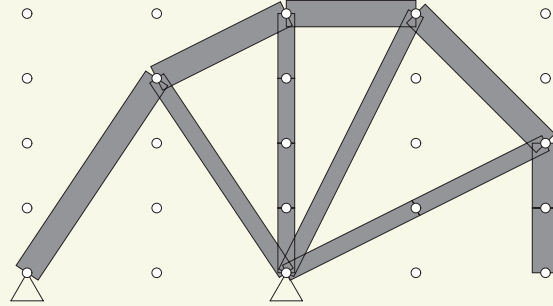
- Choose c-s areas from a set of predetermined values.
- The # of different c-s areas is (certainly) small, but...
 - ...the opt. sol. highly depends on the predetermined values.

ex.) 200-bar truss: discrete optimization

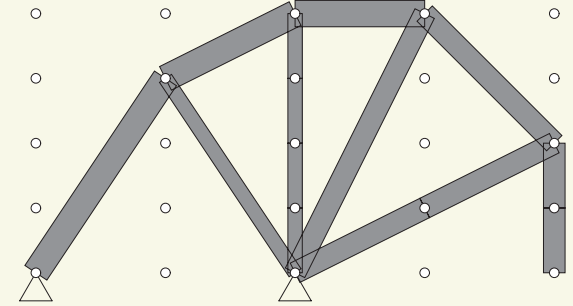
- $x_e \in \{0, 120, 240, \dots, 1875\}$: 16 candidate values
- w/ cstr. on # of different c-s areas



$n = 1$



$n = 2$

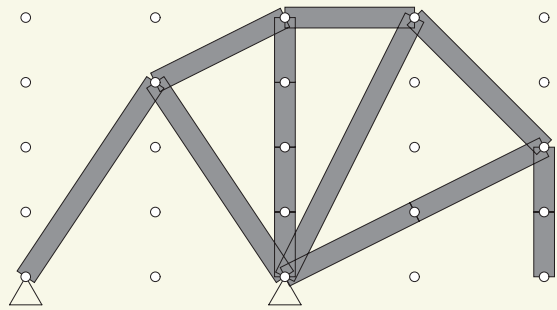


$n = 3$

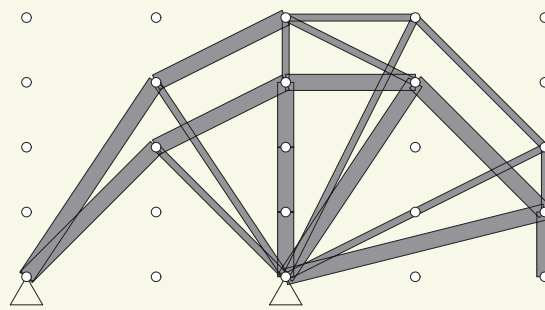
n	Time (s)
1	34.7
2	68.3
3	502.3 (< 9 min)

ex.) 200-bar truss: discrete optimization

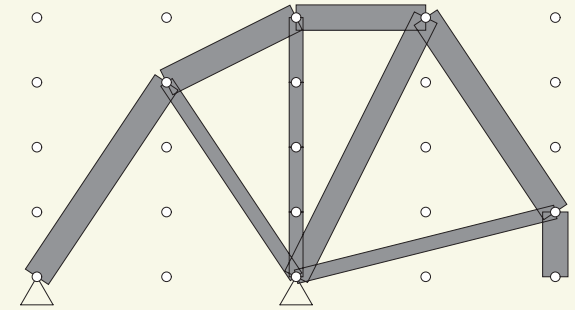
- $x_e \in \{0, 125, 250, \dots, 1800\}$: 16 candidate values
- w/ cstr. on # of different c-s areas



$n = 1$



$n = 2$



$n = 3$

n	Time (s)
1	22.8
2	139.3
3	1113.2 (< 20 min)

conclusions

- constraint on # of different design variables
 - Determine optimal values used for c-s areas, y_1, \dots, y_n .
[continuous]
 - Determine which to choose among $0, y_1, \dots, y_n$ for member e .
[combinatorial]
 - → linear ineq. with 0-1 variables
- compliance optimization of a truss
 - MISOCP (mixed-integer second-order cone programming)
 - integer variables + nonlinear convex constraints
 - global optimization
 - a branch-and-cut method (existing solvers)
 - For discrete optimization, ...
 - MISOCP is more efficient than MILP/MIQP.