

Large Deflection Analysis of Cable Networks
by Second-Order Cone Program

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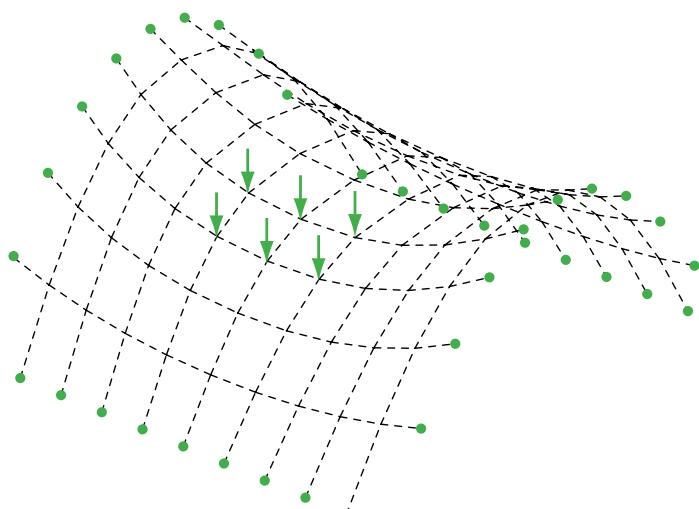
Large deformation analysis of cable network:

- Given

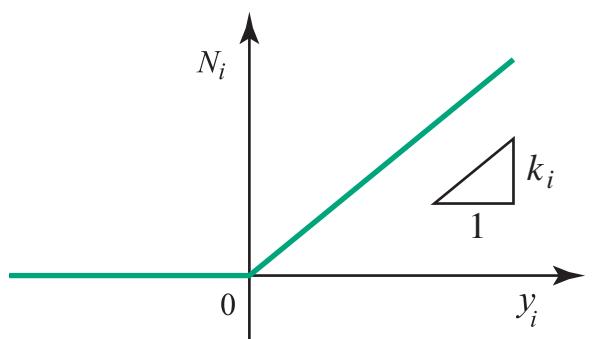
- supports : $\mathbf{b}_i^0 \in \Re^3$
- external forces : $\bar{\mathbf{f}} \in \Re^{3N^n}$
- member unstressed length : l_i^0

- Find

- internal nodes : $\mathbf{x} \in \Re^{3N^n}$



cable network



axial force—elongation

Stress unilateral behavior:

— Backgrounds: —

- transmit **only tension force**
 1. **trial-and-error**
 - (a) assume whether **in tensile** or **slackening state**
 - (b) check the obtained solution
 - (c) correct the assumption
 2. **singularity** of the tangent stiffness matrix

— The proposed algorithm: —

1. **Second-Order Cone Programming (SOCP) problem**
 \iff min. of Total Potential Energy
2. **pin-joints**, frictionless joints
3. **no assumption** on stress state
4. convergence
 - (a) **unstable** cable networks
 - (b) estimate of stress states is difficult

Second-Order Cone Programming : SOCP

1. convex programming
2. including LP, QP, etc.
3. included in SDP
4. primal-dual interior-point method
(Monteiro and Tsuchiya, 2000)
 - polynomial time convergence
5. applications
 - (a) truss topology optimization (Jarre *et al.*, 1998)
 - (b) magnetic shield design
(Sasakawa and Tsuchiya, 2000)
 - (c) antenna array design (Scholnik and Coleman, 2000)

Second-Order Cone Programming : SOCP

$$\begin{aligned} \text{Minimize} \quad & \mathbf{b}^\top \mathbf{y} \\ \text{subject to} \quad & \mathbf{A}^\top \mathbf{y} + \mathbf{x} = \mathbf{c}, \\ & x_0 \geq \|\mathbf{x}_1\|. \end{aligned}$$

Variable vectors

$$\mathbf{x} = (x_0, \mathbf{x}_1) \in \mathbb{R}^n, \quad \mathbf{y} \in \mathbb{R}^m$$

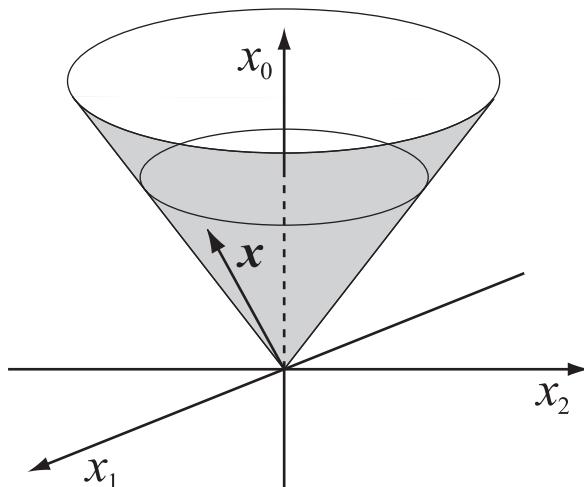
Definitions

$$\|\mathbf{x}_1\| = (\mathbf{x}_1^\top \mathbf{x}_1)^{1/2} \quad : \text{Euclidean norm}$$

$$\mathcal{K}(n) = \{(x_0, \mathbf{x}_1) | x_0 \geq \|\mathbf{x}_1\|\} \quad : \text{second-order cone}$$

Constant matrix and vectors

$$\mathbf{A} \in \mathbb{R}^{m \times n}, \quad \mathbf{b} \in \mathbb{R}^m, \quad \mathbf{c} \in \mathbb{R}^n$$



Second-order cone in 3-dimensional space

Minimization problem of TPE

$$\begin{aligned}
 \text{TPE : Minimize} \quad & \sum_{i=1}^{N^m} w_i(y_i) - \bar{\mathbf{f}}^\top \mathbf{x} \\
 \text{subject to} \quad & w_i(y_i) = \begin{cases} \frac{1}{2} k_i y_i^2, & (y_i \geq 0), \\ 0, & (y_i < 0), \end{cases} \\
 & y_i = \|\mathbf{B}_i \mathbf{x} + \mathbf{b}_i^0\| - l_i^0.
 \end{aligned}$$

Variables:

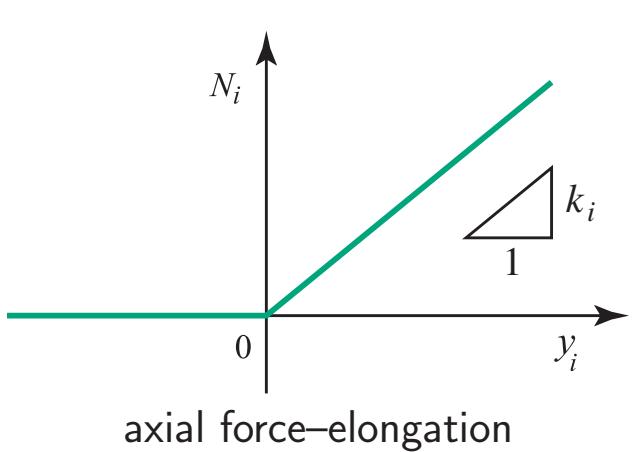
y_i : member elongation, \mathbf{x} : internal nodes

Given:

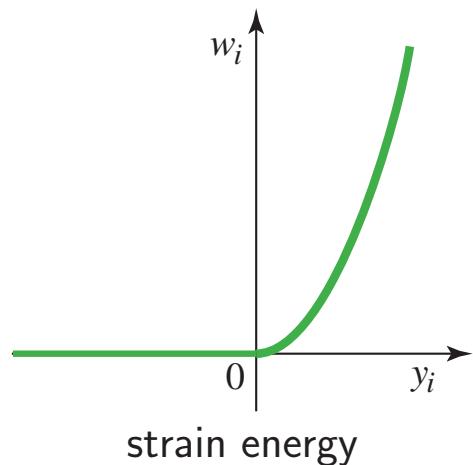
$\bar{\mathbf{f}}$: external forces, l_i^0 : member unstressed length,
 \mathbf{b}_i^0 : supports, \mathbf{B}_i^0 : adjacency matrices

Strain energy:

$w_i(y_i)$: strain energy. k_i : extensional stiffness



axial force–elongation



strain energy

1. nonconvex problem
2. w_i depends on the sign of y_i
 - assumptions are required
 - trial-and-error process

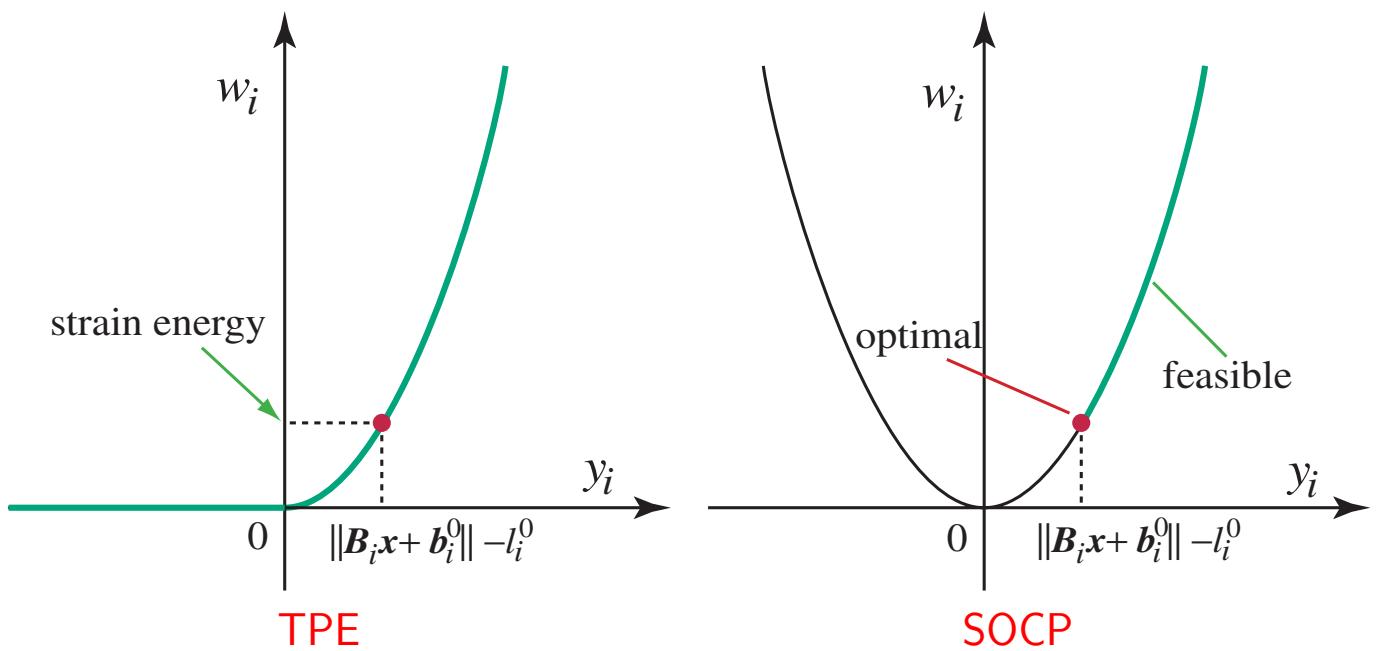
Minimization problem of TPE:

$$\begin{aligned} \text{TPE : Minimize} \quad & \sum_{i=1}^{N^m} w_i(y_i) - \bar{\mathbf{f}}^\top \mathbf{x} \\ \text{subject to} \quad & w_i(y_i) = \begin{cases} \frac{1}{2}k_i y_i^2, & (y_i \geq 0), \\ 0, & (y_i < 0), \end{cases} \\ & y_i = \|\mathbf{B}_i \mathbf{x} + \mathbf{b}_i^0\| - l_i^0. \end{aligned}$$

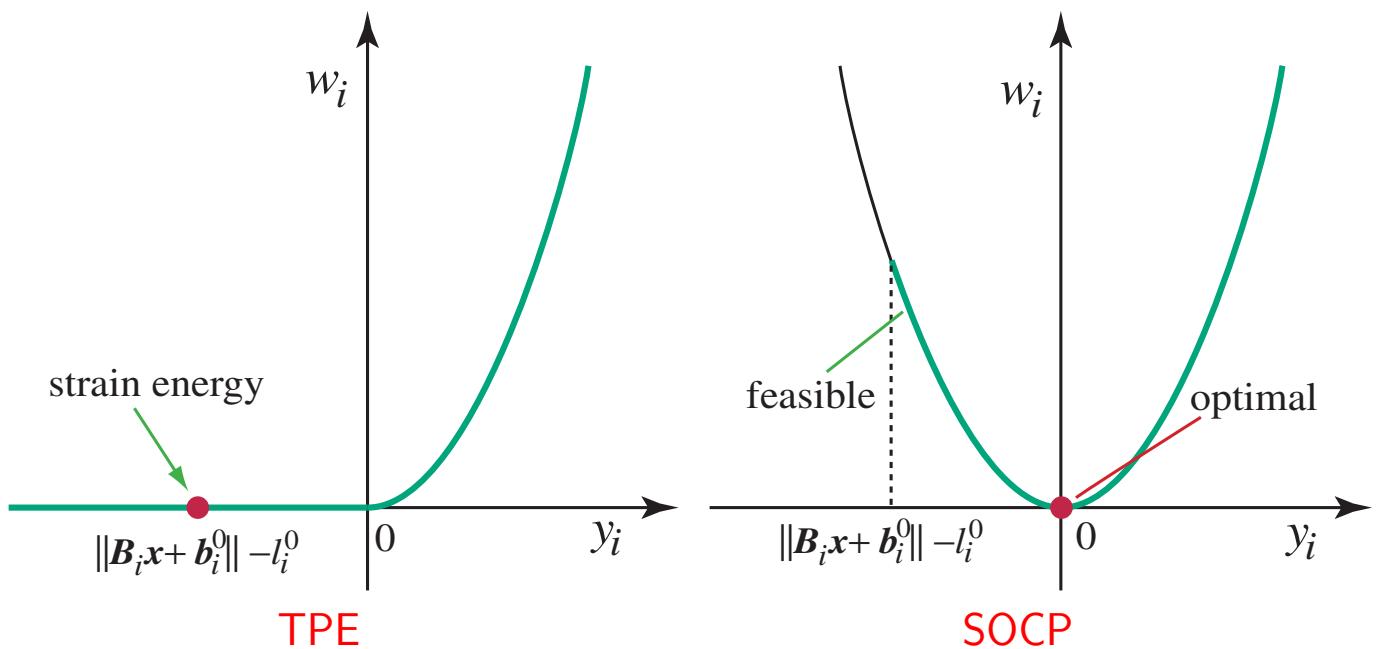
SOCP formulation:

$$\begin{aligned} \text{SOCP : Minimize} \quad & \sum_{i=1}^{N^m} \frac{1}{2} k_i y_i^2 - \bar{\mathbf{f}}^\top \mathbf{x} \\ \text{subject to} \quad & y_i \geq \|\mathbf{B}_i \mathbf{x} + \mathbf{b}_i^0\| - l_i^0. \end{aligned}$$

in tensile state :



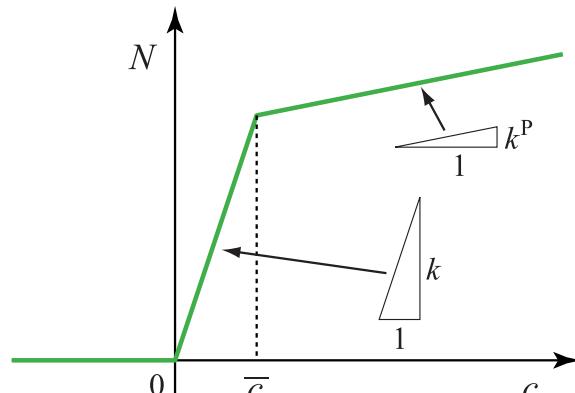
slackening :



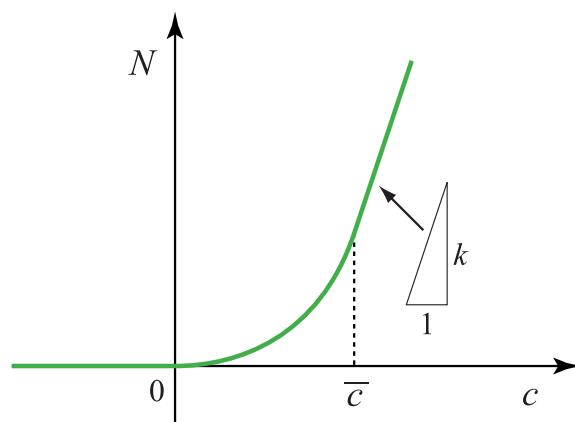
SOCP:

1. has the same optimizer as that of TPE
2. convex problem
3. efficient algorithm
 - no assumption is required—no trial-and-error process
 - polynomial-time convergence—IPM

Nonlinear constitutive law \implies SOCP:



Bi-linear material.



quadratic-linear constitutive law.

stiffness reduction:

1. small elongation
2. strand cable becomes lose
3. deflection of cable \Leftarrow own weight

Optimality conditions:

$$\text{SOCP : Minimize} \quad \sum_{i=1}^{N^m} \frac{1}{2} k_i y_i^2 - \bar{\mathbf{f}}^\top \mathbf{x}$$

$$\text{subject to} \quad y_i \geq \|\mathbf{B}_i \mathbf{x} + \mathbf{b}_i^0\| - l_i^0.$$

Lagrangian multipliers

$$q_i \in \Re, \quad \mathbf{v}_i \in \Re^3, \quad (i = 1, 2, \dots, N^m).$$

KKT conditions:

$$q_i = k_i y_i, \quad : \text{constitutive law}$$

$$\sum_{i=1}^{N^m} \mathbf{B}_i^\top \mathbf{v}_i + \bar{\mathbf{f}} = \mathbf{0}, \quad : \text{equilibrium equations}$$

$$(y_i + \bar{l}_i^0) q_i + (\mathbf{B}_i \mathbf{x} + \mathbf{b}_i^0)^\top \mathbf{v}_i = 0,$$

$$y_i \geq \|\mathbf{B}_i \mathbf{x} + \mathbf{b}_i^0\| - \bar{l}_i^0, \quad q_i \geq \|\mathbf{v}_i\|.$$

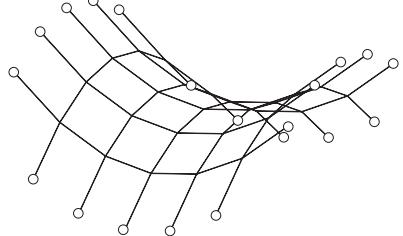
- q_i : axial force
- \mathbf{v}_i : internal force vector

Examples:

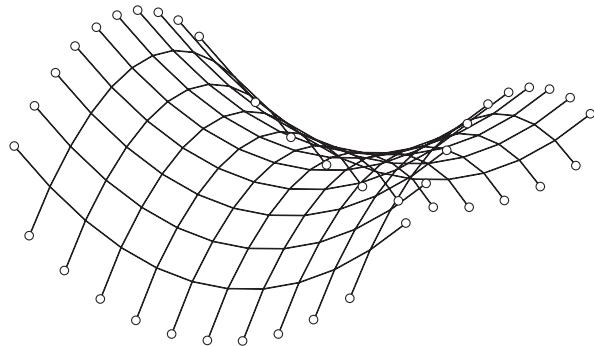
SOCP : solve SOCP problem by IPM.

TPE : solve min. of TPE by IPM.

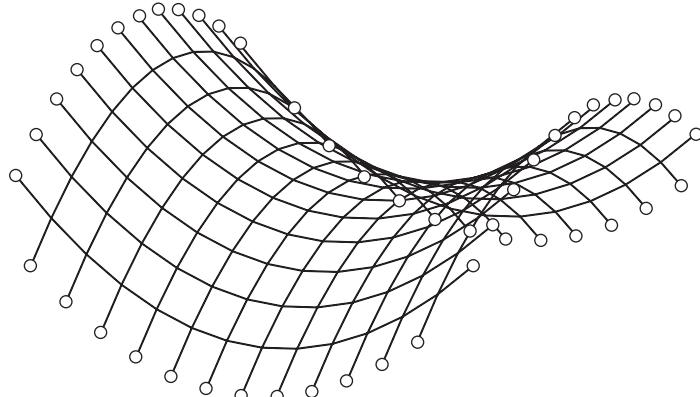
NR : Newton-Raphson method (tangent stiffness).



Model (I)



Model (II)



Model (III)

Self-equilibrium shape analysis

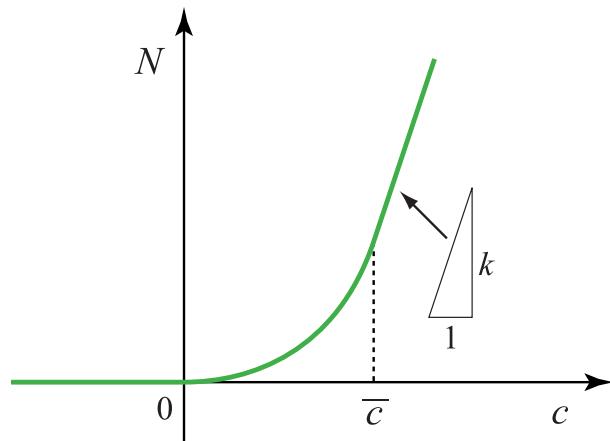
algorithm	model		steps	CPU time (sec.)	
	#	n		total	ave.
SOCP	(I)	195	11	0.23	0.021
	(II)	740	14	1.42	0.101
	(III)	1056	15	2.46	0.164
TPE	(I)	135	22	0.50	0.023
	(II)	520	22	2.44	0.111
	(III)	744	22	3.81	0.173
NR	(I)	75	19	0.28	0.014
	(II)	300	22	4.71	0.214
	(III)	432	22	20.31	0.923

1. CPU time

- $\mathcal{O}(n) < \text{SOCP} < \text{TPE} < \mathcal{O}(n^2)$
- $\mathcal{O}(n^2) < \text{NR} < \mathcal{O}(n^3)$

2. # of variables : n

- $\text{SOCP} > \text{TPE} > \text{NR}$



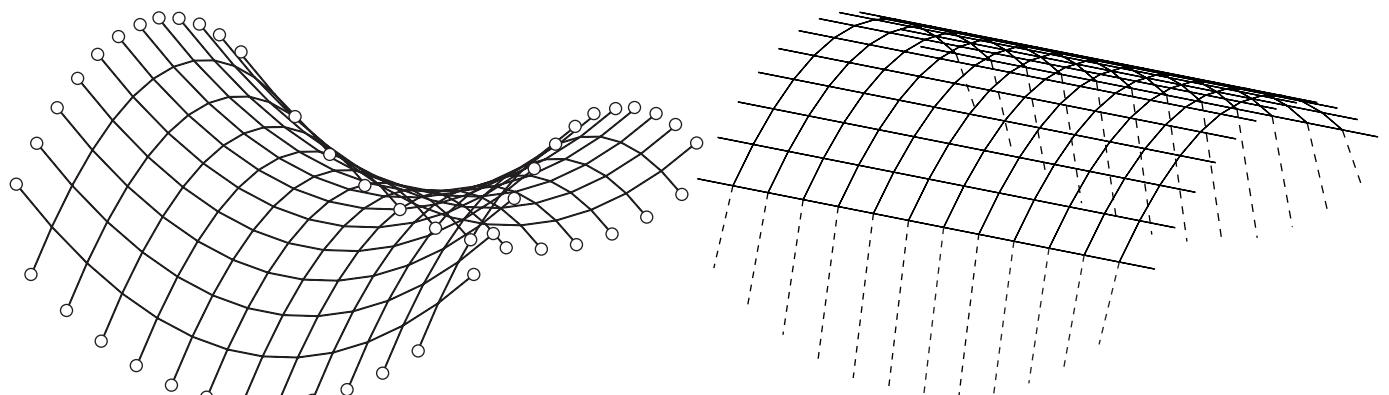
Dependence of initial solutions

algorithm	model	(A)			(B)	
		#	n	steps	CPU (sec.)	steps
SOCP	(I)	135		11	0.21	15
	(II)	520		11	0.90	15
	(III)	744		11	1.42	23
TPE	(I)	135		11	0.24	15
	(II)	520		11	0.93	15
	(III)	744		15	2.10	31
NR	(I)	75		22	0.26	*
	(II)	300		20	4.24	*
	(III)	432		9	7.40	*

1. SOCP (A) ≈ SOCP (B)

2. NR (B) : fail

tangent stiffness matrix : singular



Initial solution (A).

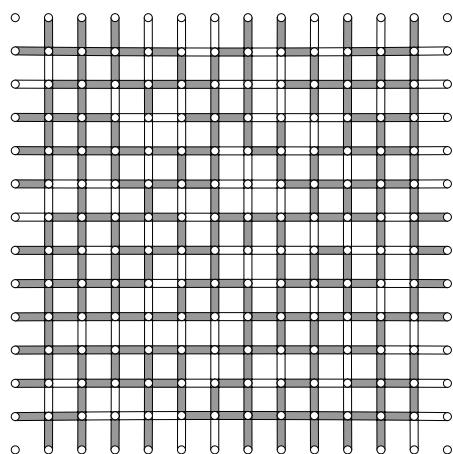
Initial solution (B).

Initial configuration with many slackening members

algorithm	model constitutive law	n	steps	CPU time (sec.)	
				total	ave.
SOCP	linear	744	45	5.37	0.120
SOCP	quadratic	1056	34	5.26	0.155
TPE	linear	744	51	6.37	0.125
TPE	quadratic	744	**	**	0.978
NR	linear	432	**	**	0.873
NR	quadratic	432	**	**	1.122

** : did not converge within 1000 steps.

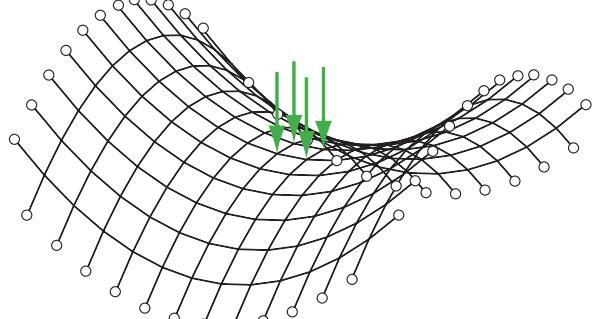
1. SOCP : converge
2. TPE, NR : fail (oscillation)
 - trial-and-error process



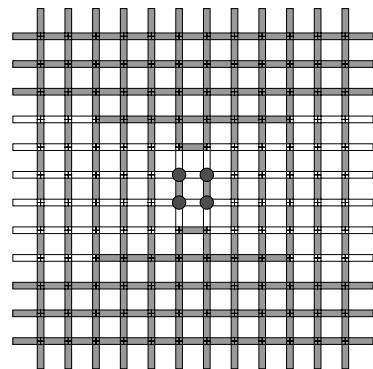
Model (III'): Slackening members.

Bi-linear material

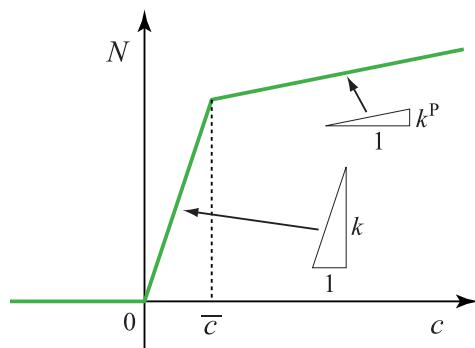
algorithm	model		steps	CPU time (sec.)	
	#	n		total	ave.
SOCP	(I)	195	10	0.44	0.044
	(II)	740	10	1.39	0.139
	(III)	1056	10	2.06	0.206
TPE	(I)	135	10	0.58	0.058
	(II)	520	11	1.62	0.147
	(III)	774	11	2.17	0.197
NR	(I)	75	25	0.32	0.013
	(II)	300	32	6.92	0.194
	(III)	432	34	31.66	0.931



External loads.



Members in plastic state



Conclusions:

1. An **SOCP formulation** has been proposed for large deformation analysis of cable networks.
 - (a) **pin-joints**
 - (b) **frictionless joints**
 - (c) **nonlinear material**
2. Equilibrium configurations are obtained by solving SOCP problems by using **Interior Point Method**.
 - (a) **no assumption** on stress state
 - (b) no process of **trial and error**
3. SOCP formulation is **more efficient** than
 - (a) min. of **Total Potential Energy**.
 - (b) **Newton-Raphson method** based on tangent stiffness.